

## TRANSFORMER

Q1. Derive the expression for emf equation of a transformer.

Ans. Consider a transformer having,

$N_1$  = No. of turns in primary,

$N_2$  = No. of turns in secondary,

$E_1$  = Induced emf in primary,

$E_2$  = induced emf in secondary,

$\phi_m$  = maximum flux in core =  $B_m \times A$

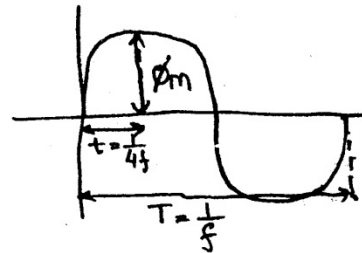
$B_m$  = maximum flux density,

$A$  = Area of the core,

$f$  = Frequency of ac input.

For maximum flux, time =  $\frac{T}{4} = \frac{1}{4f}$

$$\begin{aligned} \text{Average rate of change of flux} \\ = \frac{\phi_m}{t} = \frac{\phi_m}{\frac{1}{4f}} = 4f\phi_m \end{aligned}$$



For sinusoidal signal,

$$\text{Form factor} = \frac{\text{rms value}}{\text{average value}} = 1.11$$

$$\begin{aligned} \therefore \text{rms value/turn} &= 1.11 \times \text{average value/turn} \\ &= 1.11 \times \text{average rate of change of flux} \\ &= 1.11 \times 4f\phi_m = 4.44 f\phi_m \end{aligned}$$

$$\therefore \text{rms value of induced emf in primary} = \text{rms value/turn} \times \text{No. of turns in primary}$$

$$\therefore E_1 = 4.44 f\phi_m \times N_1 = 4.44 f N_1 B_m A$$

Similarly,  $E_2 = 4.44 f N_2 B_m A$  (where  $\phi_m = B_m \cdot A$ )

NOTE: (1)  $\frac{E_1}{N_1} = \frac{E_2}{N_2} = 4.44 f \phi_m$

∴ Emf/turn is same in both primary & secondary winding.

(2) For ideal transformer,  $V_1 = E_1$  &  $V_2 = E_2$  where  $V_1$  &  $V_2$  are terminal voltages.

(3)  $\frac{E_2}{E_1} = \frac{N_2}{N_1} = k$ ; where  $k =$  voltage transformation ratio

If  $N_2 > N_1$ , then  $k > 1$  for step up transformer,

If  $N_1 > N_2$  then  $k < 1$  for step down transformer.

(4) For ideal transformer, efficiency = 100%,

∴ Input VA = Output VA

$$\therefore V_1 I_1 = V_2 I_2$$

$$\therefore \frac{V_2}{V_1} = \frac{I_1}{I_2}$$

$$\therefore \boxed{\frac{V_2}{V_1} = \frac{E_2}{E_1} = \frac{N_2}{N_1} = \frac{I_1}{I_2} = k} \quad (\text{For ideal transformer})$$

Q2) Transformer On No-load:

At no-load, the primary input current has to supply

(i) Iron losses in core i.e. eddy current loss & hysteresis loss

(ii) Small amount of copper loss in primary.

Thus  $I_0$  lags  $V_1$  by an angle  $\phi_0 < 90^\circ$ .

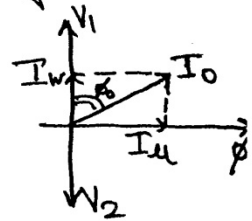
$$\text{Input power} = W_0 = V_1 I_0 \cos \phi_0 = V_1 I_w$$

From vector diag,  $I_0$  has two components -

(i)  $I_w = I_0 \cos \phi_0$ ; is in phase with  $V_1$  & supplies iron loss & copper loss & is known as active or working or iron loss component

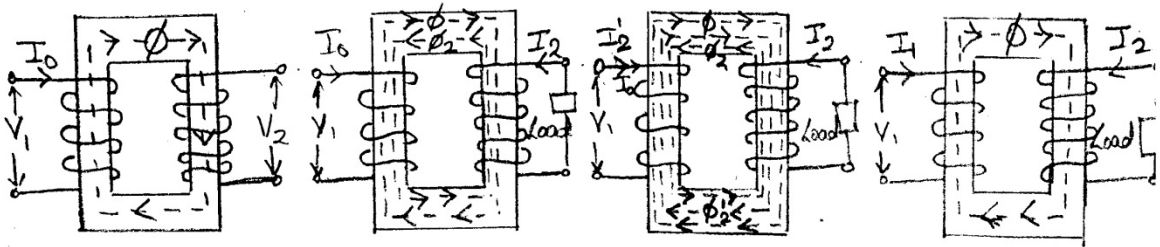
(ii)  $I_m = I_0 \sin \phi_0$ ; is in quadrature with  $V_1$  & sustains the alternating flux in the core & is known as magnetising or wattless component.

$$\therefore I_0 = \sqrt{I_m^2 + I_w^2} \quad \& \quad \phi_0 = \text{hysteresis } \& \text{ of advance}$$



## Transformer On load:

When the secondary is loaded, secondary current  $I_2$  is set up.  $I_2$  is in phase with  $V_2$  if load is non-inductive, it lags if load is inductive & leads if load is capacitive.

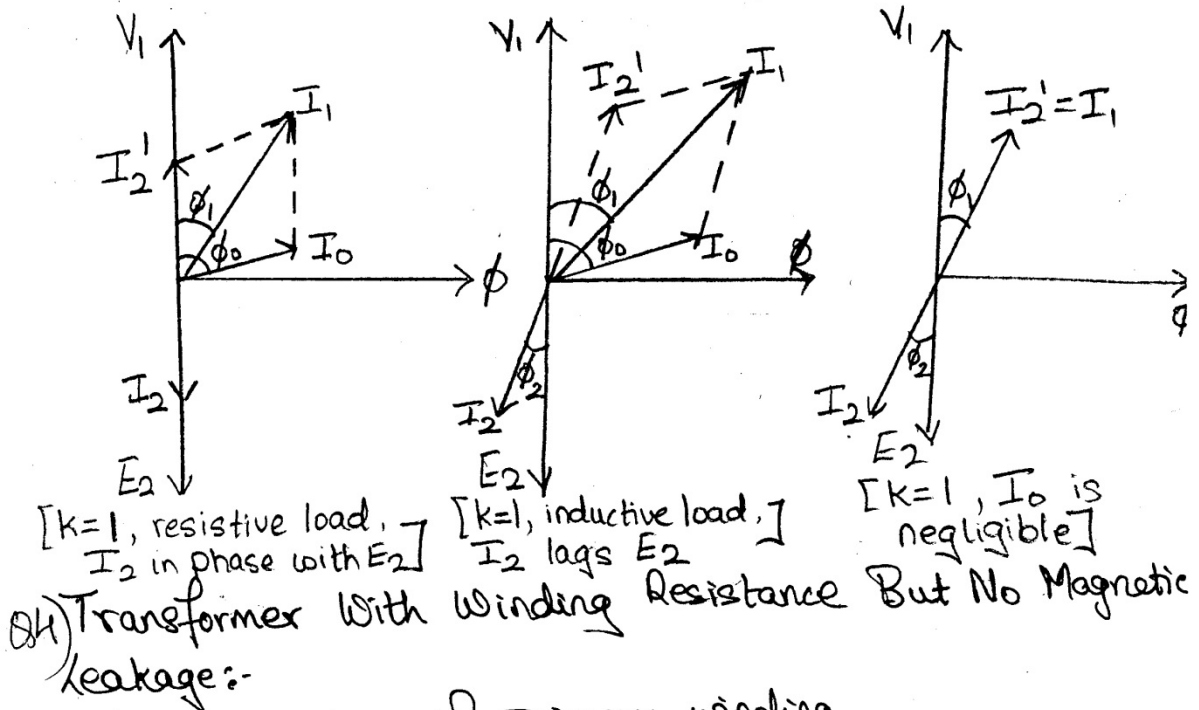


The secondary current sets up its own flux  $\phi_2$  which is in opposition to the main primary flux  $\phi$  which is due to  $I_0$ . The opposing secondary flux  $\phi_2$  weakens the primary flux  $\phi$  momentarily, hence primary back emf  $E_1$  tends to be reduced. For a moment  $V_1$  gains the upper hand over  $E_1$  & hence causes more current to flow in primary. This current  $I_2'$  is known as the load component of primary current and is in antiphase with  $I_2$ . It sets its own flux  $\phi_2'$  in opposition to flux  $\phi_2$ . Since  $\phi_2$  &  $\phi_2'$  are equal in magnitude but opposite in direction they cancel off each other. Thus the magnetic effect of  $I_2$  is neutralised by  $I_2'$ . Thus the net flux passing through the core is approximately the same as at no-load.

$$\text{As } \phi_2 = \phi_2' \therefore N_2 I_2 = N_1 I_2' \therefore I_2' = \frac{N_2}{N_1} \cdot I_2$$

$$\therefore \boxed{I_2' = k I_2} \therefore \frac{I_2'}{I_2} = k.$$

When transformer is on no-load, the primary current is the vector sum of  $I_0$  &  $I_2'$ .



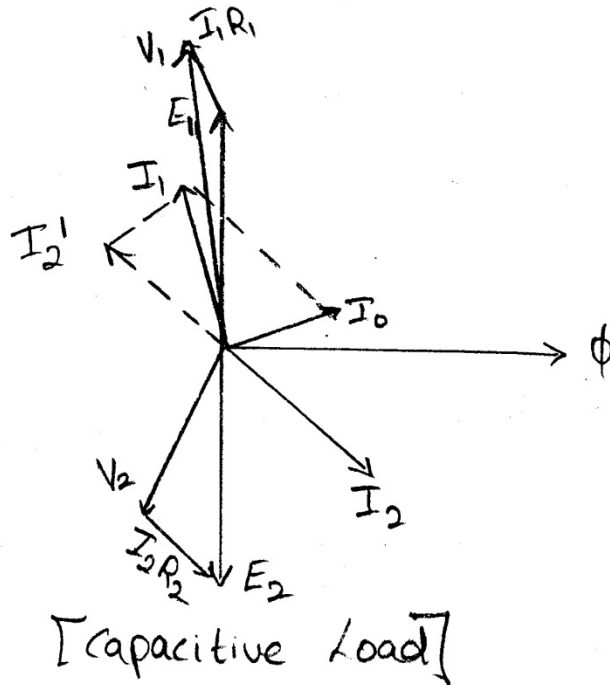
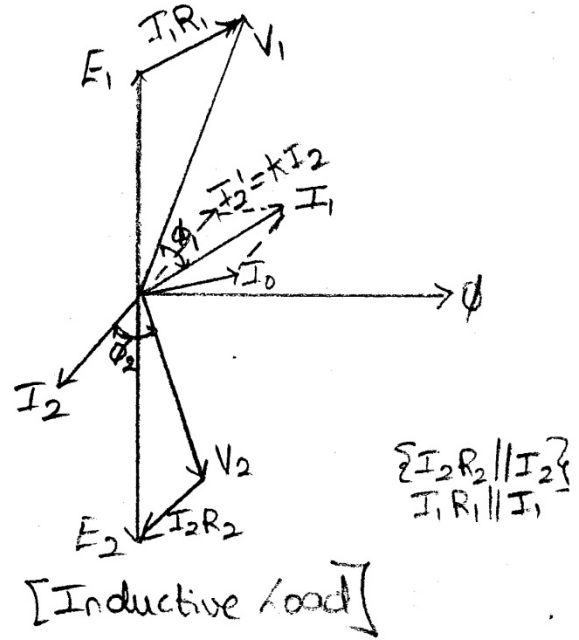
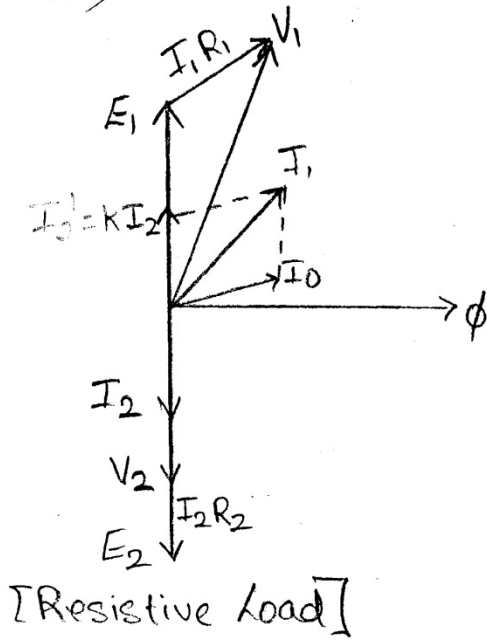
- If  $R_1$  = resistance of primary winding,
- $R_2$  = resistance of secondary winding.
- $E_1$  = primary induced emf,
- $E_2$  = secondary induced emf,
- $V_1$  = Terminal voltage of primary,
- $V_2$  = Terminal voltage of secondary,
- $I_1$  = Primary current,
- $I_2$  = Secondary current.

Then,

$$\begin{cases} E_2 - V_2 = I_2 R_2 \\ V_1 - E_1 = I_1 R_1 \end{cases}$$

If  $R_2'$  = equivalent secondary resistance as referred to primary,  
 Then,  $R_2'$  in primary would cause the same loss as  $R_2$  in the secondary

Q7)



$$I_1^2 R_2' = I_2^2 R_2$$

$$\therefore R_2' = \left(\frac{I_2}{I_1}\right)^2 \cdot R_2$$

$$\therefore R_2' = \frac{R_2}{K^2}$$

$$\left\{ \because \frac{I_2}{I_1} = \frac{1}{K} \right\}$$

When component from secondary is shifted to primary then we divide by  $K^2$

$\therefore$  Equivalent or effective resistance of the transformer as referred to primary is,

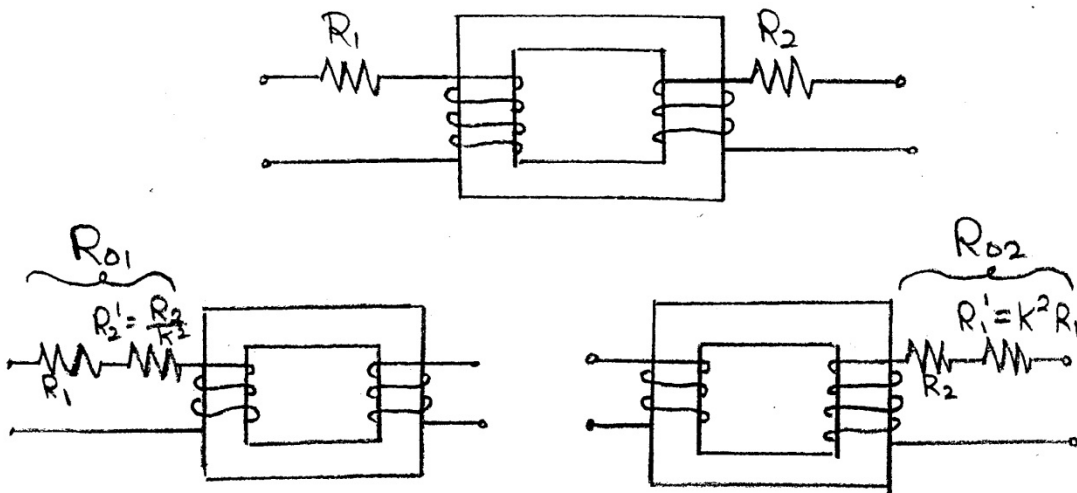
$$R_{01} = R_1 + R_2' = R_1 + \frac{R_2}{K^2}$$

Similarly, if  $R_1'$  = equivalent primary resistance as referred to secondary,

$$\therefore R_1' = K^2 R_1$$

When component from primary is shifted to secondary then we multiply by  $K^2$

$$\therefore R_{02} = R_2 + R_1' = R_2 + K^2 R_1$$

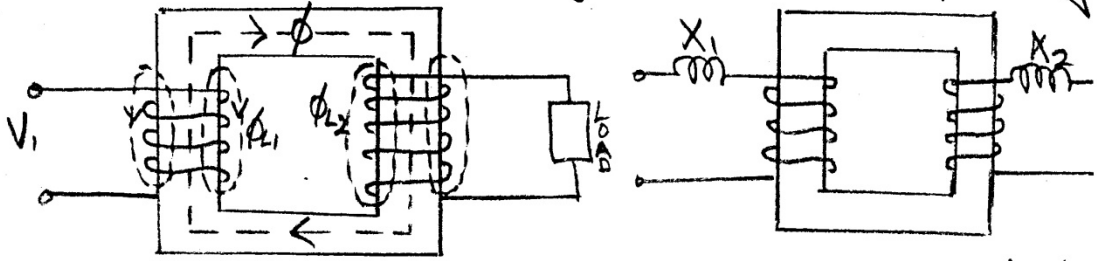


Q.2)

**Magnetic leakage:**

All flux linked with primary does not link the secondary but part of it i.e.  $\phi_L$  completes its magnetic circuit by passing through air rather than around the core. This primary leakage flux induces an emf  $e_L$ .

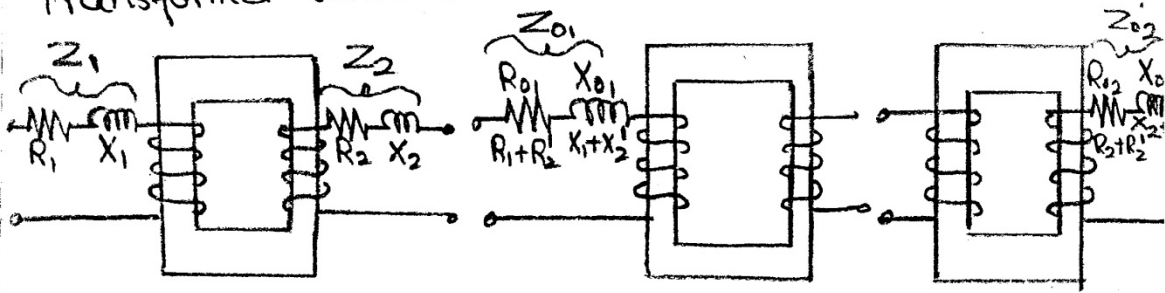
In the primary but not in secondary. Similarly  $\phi_{L2}$  induces emf in the secondary  $E_{L2}$  but not in primary



A transformer with magnetic leakage is equivalent to an ideal transformer with inductive coils connected in both primary & secondary circuits such that emf in each coil is equal to that due to the corresponding leakage flux in actual transformer.

$$\therefore X_1 = \frac{E_{L1}}{I_1} \quad \& \quad I_2 X_2 = \frac{E_{L2}}{I_2}$$

Q6) Transformer with Resistance & leakage reactance:



Primary impedance,  $Z_1 = \sqrt{R_1^2 + X_1^2}$

Secondary impedance,  $Z_2 = \sqrt{R_2^2 + X_2^2}$

$$V_1 = E_1 + I_1(R_1 + jX_1) = E_1 + I_1 Z_1$$

$$E_2 = V_2 + I_2(R_2 + jX_2) = V_2 + I_2 Z_2$$

$$X_{01} = X_1 + X_2' = X_1 + X_2/k^2 \quad ; \quad R_{01} = R_1 + R_2' = R_1 + R_2/k^2$$

$$X_{02} = X_2 + X_1' = X_2 + k^2 X_1 \quad ; \quad R_{02} = R_2 + R_1' = R_2 + k^2 R_1$$

$$\therefore Z_{01} = \sqrt{R_{01}^2 + X_{01}^2} \quad \& \quad Z_{02} = \sqrt{R_{02}^2 + X_{02}^2}$$

